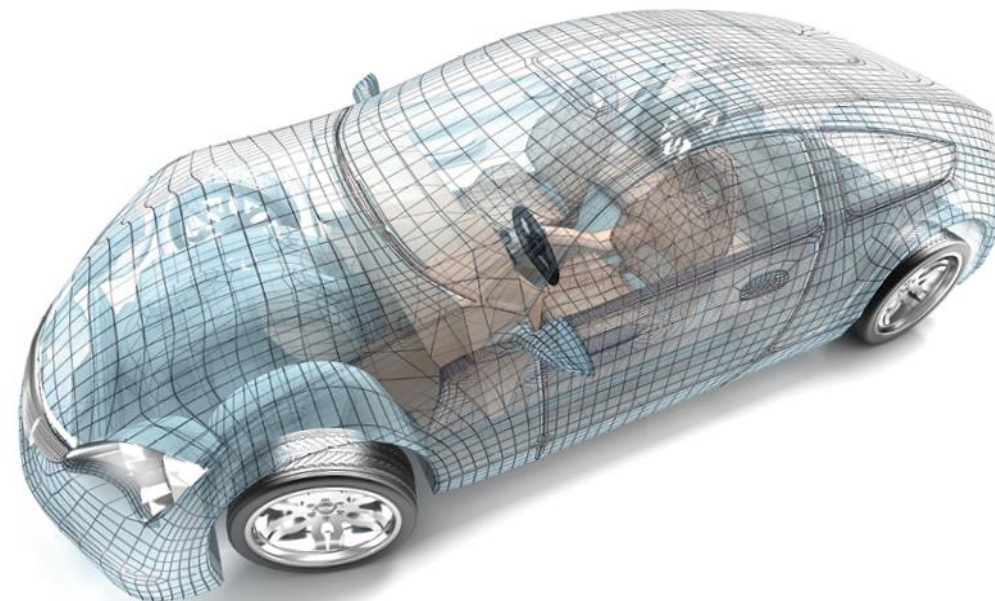




**THERMOPLASTIC
COMPOSITES CONFERENCE**

**A VIRTUAL EVENT
APRIL 29 - MAY 1, 2020**



Using process simulation for the advanced forming of a thermoplastic composite part

Presented By: Thijs Donderwinkel, AniForm Engineering
In collaboration with: Noushin Bahramshahi, Collins Aerospace

PRESENTED BY



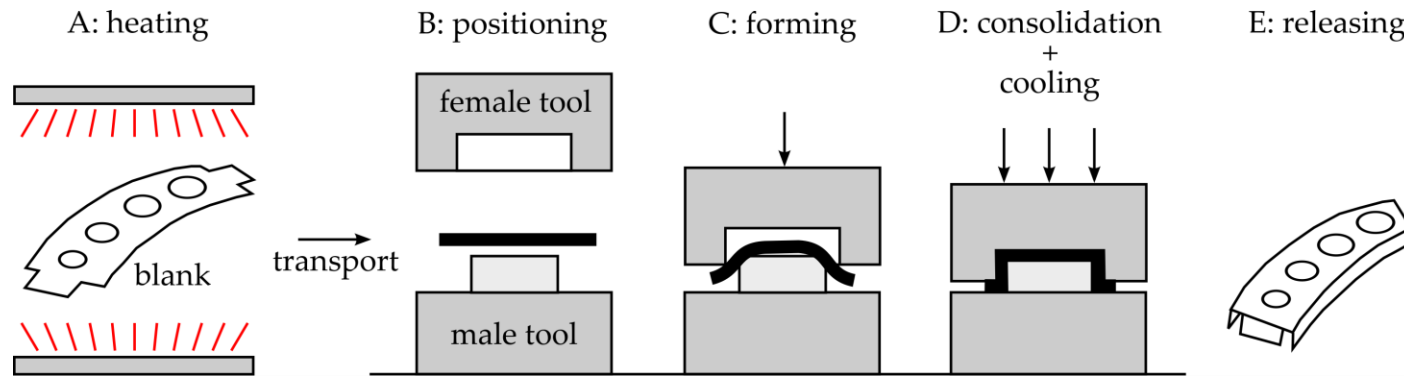
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Introduction

Stamp forming process

- Pre-consolidated laminate heated in IR oven
- Laminate transport to press
- Tool closes to form and (re)-consolidation the product



- Short cycle times
- High mechanical performance
- Cost reduction via high volume production and automation

Introduction

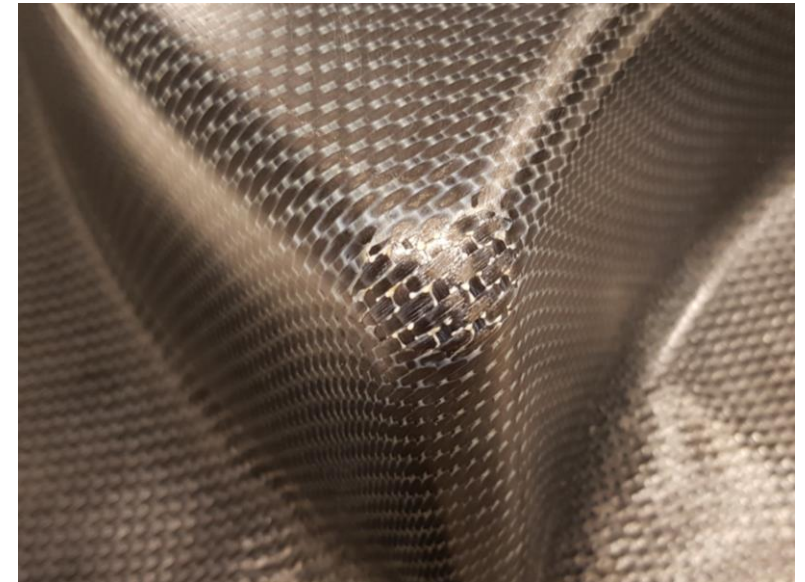
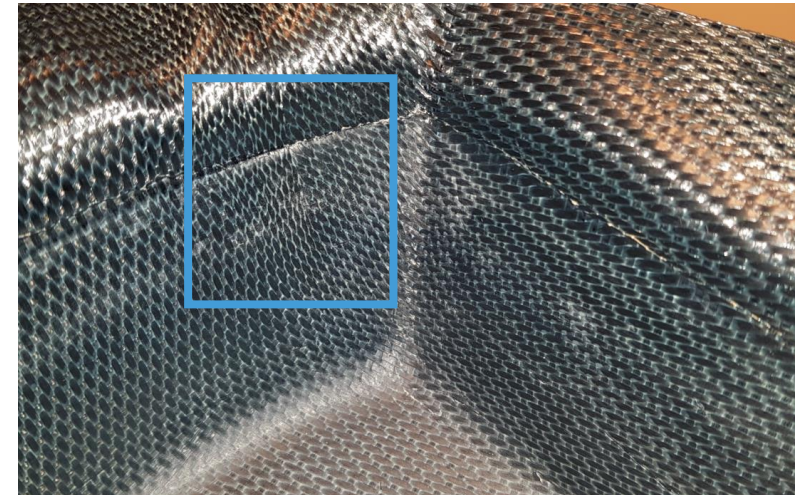
Typical challenges for composite stamp forming:

- forming-induced deformation and resulting thickness change;
- wrinkle formation as a result of excessive shearing and/or fiber compression;
- consolidation issues because of fiber tensioning and thickness changes;
- blank misalignment issues and laminate contour optimization for formability.

State-of-the-art simulation techniques:

- provide a better understanding of frequently occurring adverse phenomena in the forming process;
- enable efficiently the study of potentially resolving process configurations;
- contribute to finding the optimal process solution.

ANIFORM's simulation technology supports these design efforts



Case study overview

Demonstrate state-of-the-art technology by:

Case 1 - Large aerospace part

- Study the formability and forming-induced effects as a function of part-size

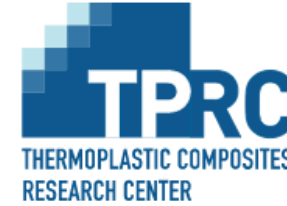
Case 2 - Overmolding demonstrator

- Determine near net-shape laminare contour and identify potential blank alignment issues in a closed cavity

Case 3 – Deep box with concave & convex flanges

- Optimize for minimal wrinkle formation

Case study 1 – Large aerospace part

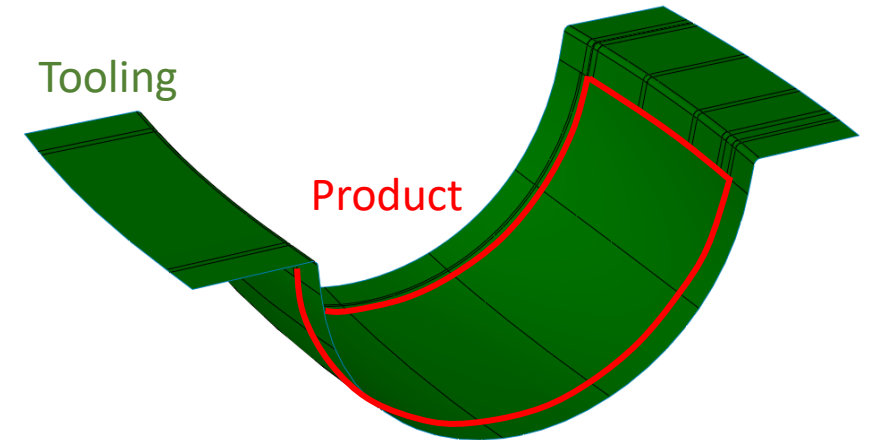


Goal

- Study the formability and forming-induced effects as a function of part-size

Simulation setup

- Toray Cetex® TC1225 (carbon fiber/PAEK) unidirectional tape
- Laminate
 - 11 plies, quasi-isotropic layup
 - Dimensions 5800 x 2500 mm
- Closing speed 1000 mm/s

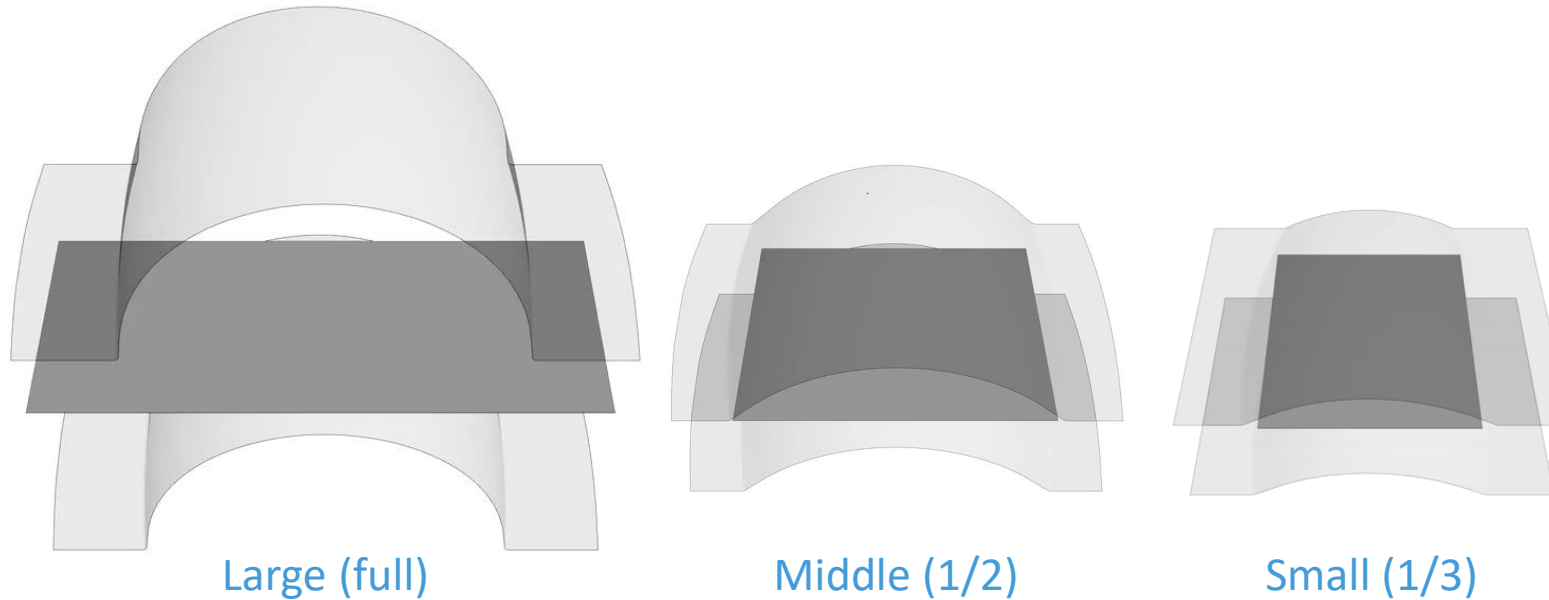


Case study 1 – Large aerospace part



Scalability study

- How does the deformation and resulting fiber stress scale with the product dimension?
- Deformation of laminate is primarily single curved (cylinder-like)
- Double curvature is introduced in the last steps

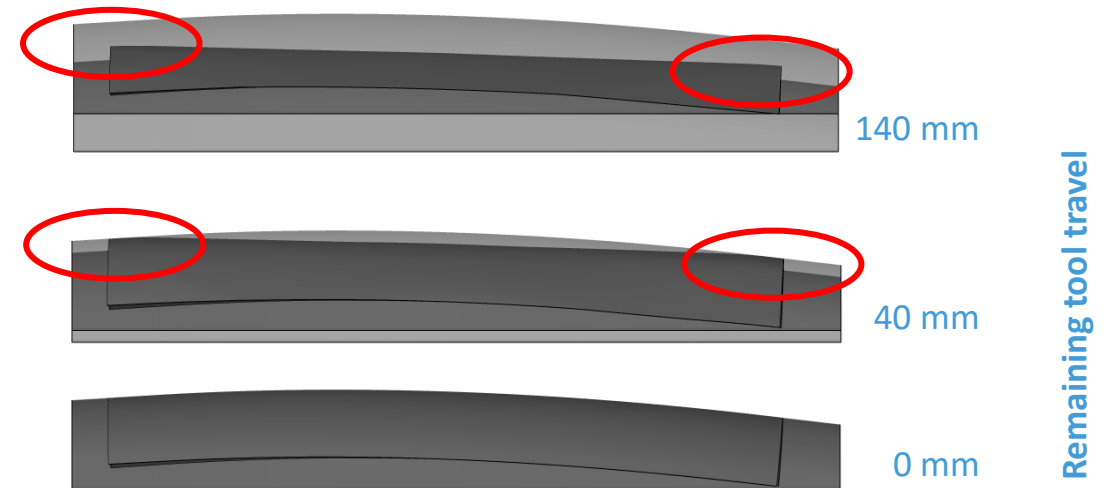


Case study 1 – Large aerospace part

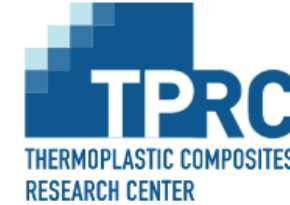


Scalability study

- Near the edge of the laminate excess material is present
 - In-plane shear might resolve the excess material



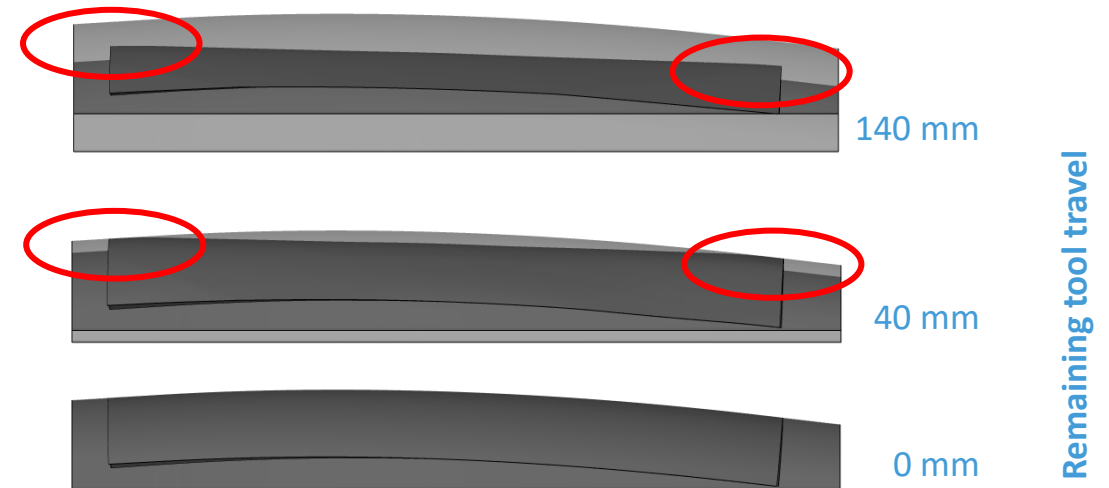
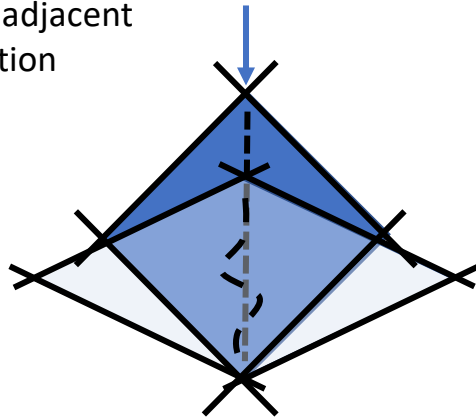
Case study 1 – Large aerospace part



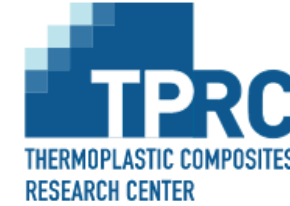
Scalability study

- Near the edge of the laminate excess material is present
 - In-plane shear might resolve the excess material
 - Quasi-isotropic impedes mobility since a fiber direction is present in the shearing direction
 - Compressive stresses arise in this region, which indicates the possible formation of wrinkles

Fiber compaction in adjacent ply in shearing direction

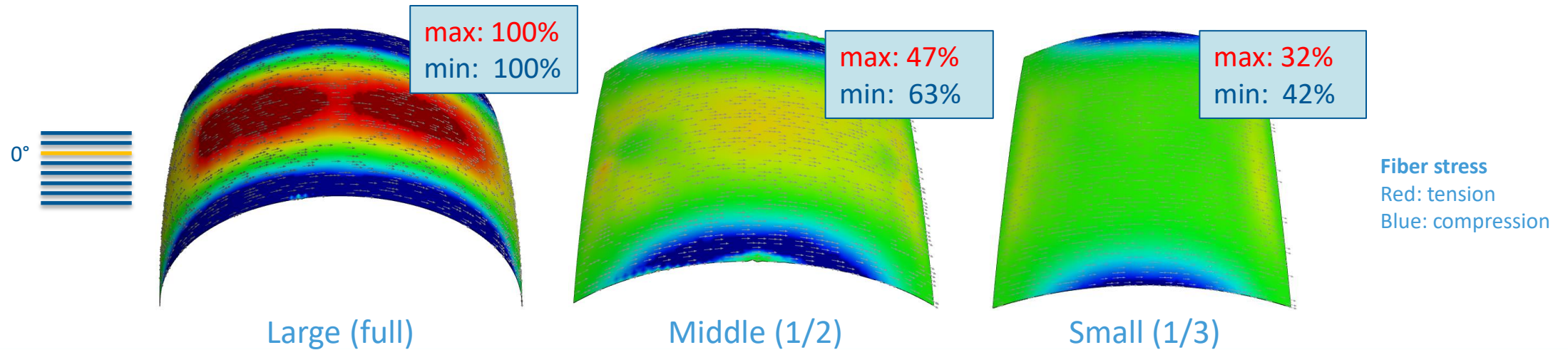


Case study 1 – Large aerospace part

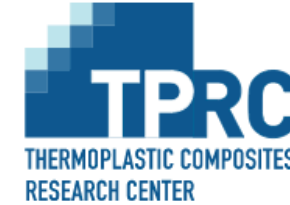


Scalability study

- Compressive stresses reduce with decreasing part size; however they are still high and indicate possible wrinkling
- High fiber tensile stresses are observed in the third (0°), which indicate possible consolidation issues (fiber migration)
 - Decreasing the part size results in a large reduction of fiber tensioning
 - Thickness increase due to surface traction (and consequent in-plane shear) is reduced, thereby increasing the mobility of the laminate

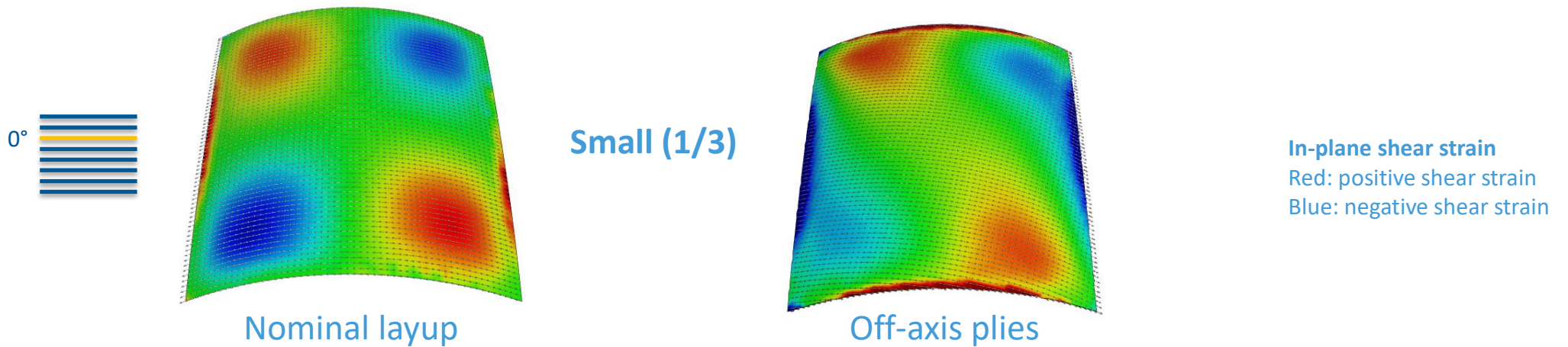


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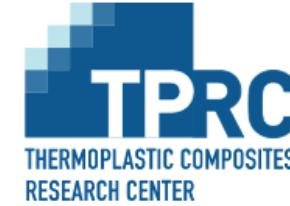


Formability improvements

- Compressive fiber stresses could be resolved by tensioning the laminate using springs
 - High mass of the laminate would require very stiff springs, which might tear the laminate in melt
 - Suitable handling system needs to be investigated
- Promote in-plane shearing in the laminate
 - Decoupling of the fiber directions: two 0° plies translate into two off-axis plies
 - Shear strain increases near the edge, which indicates improvement of mobility

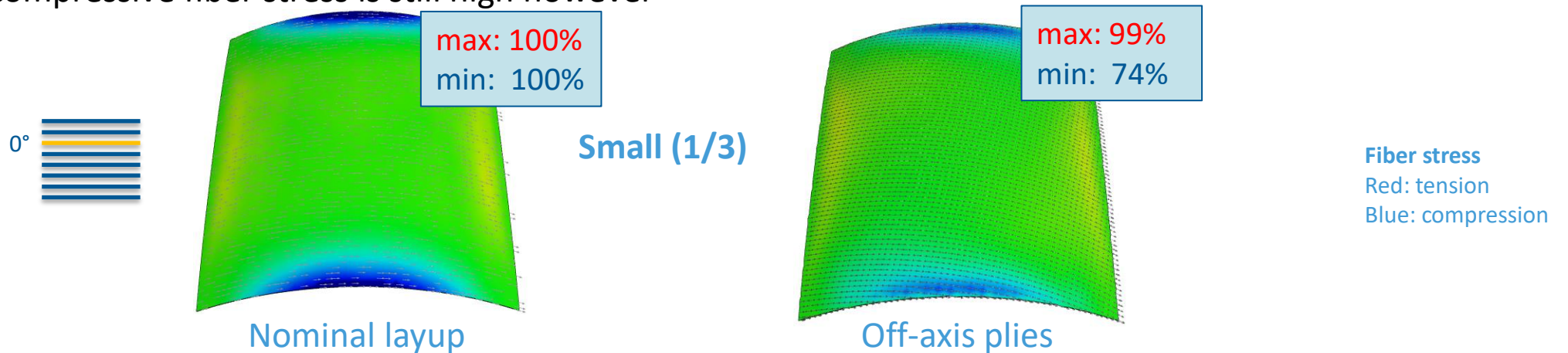


Case study 1 – Large aerospace part

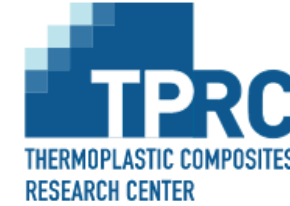


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 - Resulting compressive fiber stress is still high however

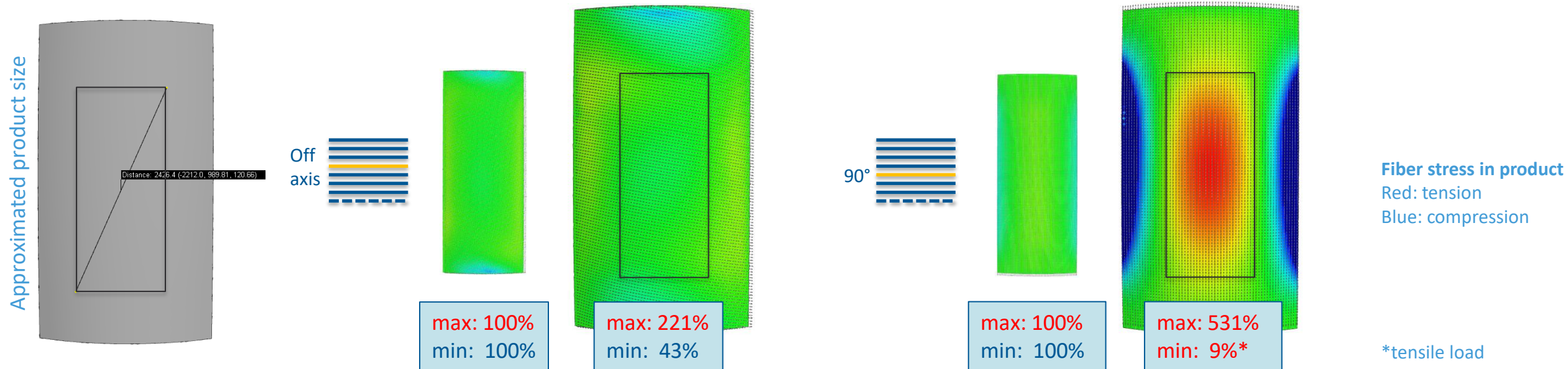


Case study 1 – Large aerospace part

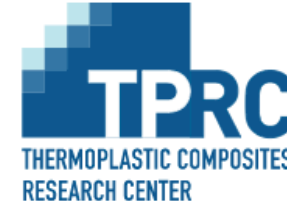


Formability improvements

- Increasing laminate size such that compressive stress are outside the product area
 - Significantly decreases the compressive stress in the plies, however tensile fiber stresses increase which indicate possible consolidation issues
- Optimize laminate dimensions is possible via the usage of simulation tools



Case study 1 – Large aerospace part



Formability improvements

- Increasing laminate size such that compressive stress are outside the product area
 - Significantly decreases the compressive stress in the plies, however tensile fiber stresses increase which indicate possible consolidation issues
- Optimize laminate dimensions is possible via the usage of simulation tools

Simulation tool supported

- Identification of potential critical fiber tensioning and compression
- Its sensitivity to part-size

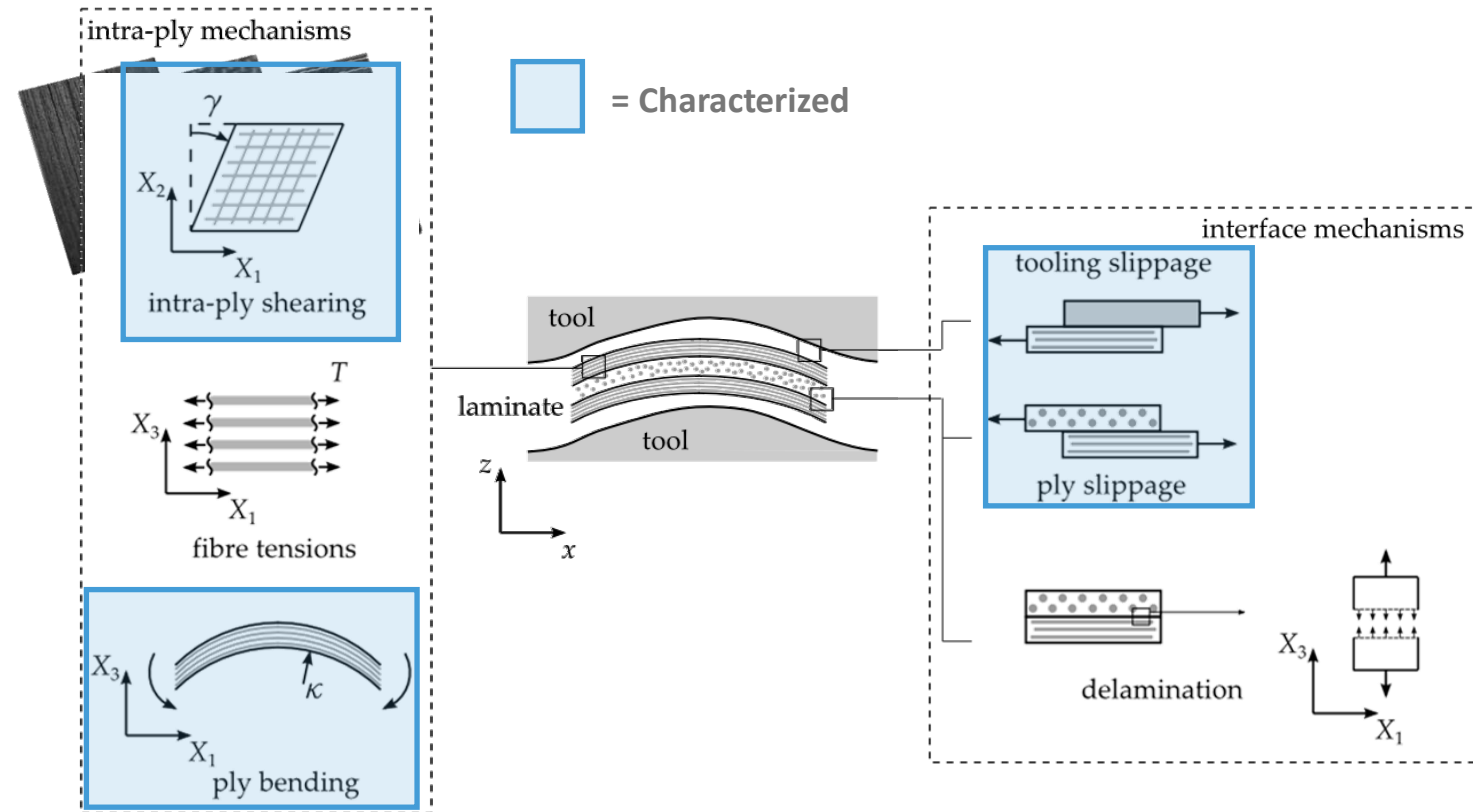
Sound understanding to support future steps

Material characterization

Various composite material types

- Unidirectional tapes
- Woven fabrics
 - Dry or thermoplastic/thermoset matrix
- Non-Crimp Fabrics

Deformation mechanisms of fiber reinforced laminated composites



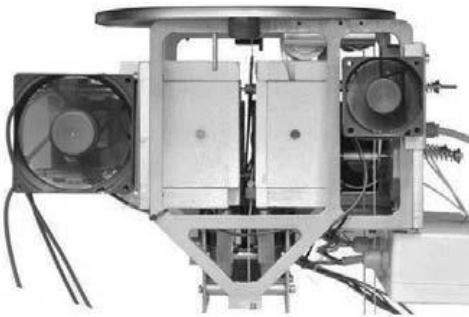
Material characterization

Characterization methods developed in collaboration with the University of Twente and TPRC

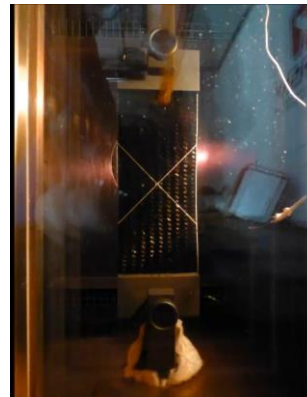
- Conditions relevant to the process
- Elevated temperatures typically above the melting temperature
- Various strain-rates relevant for the process

UNIVERSITY
OF TWENTE.

TPRC
THERMOPLASTIC COMPOSITES
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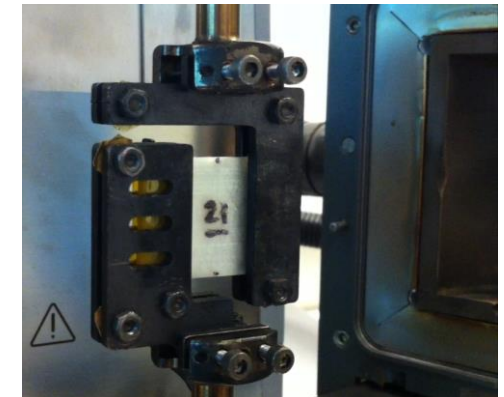
Friction



Fabric shear



Tape shear



Bending

Case study 2 – Overmolding demonstrator



Overmolding project at TPRC (COMPETE)

- Combined stamp forming and injection molding
- Function integration & net-shape manufacturing

Goal

- Determine near net-shape laminates contour and identify potential blank alignment issues in a closed cavity

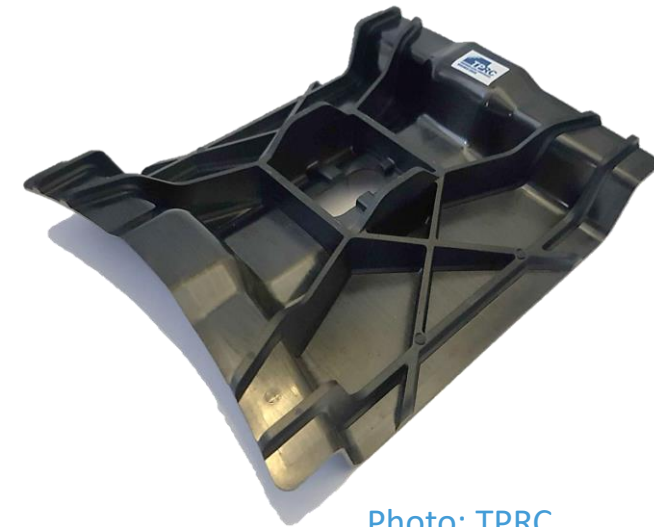
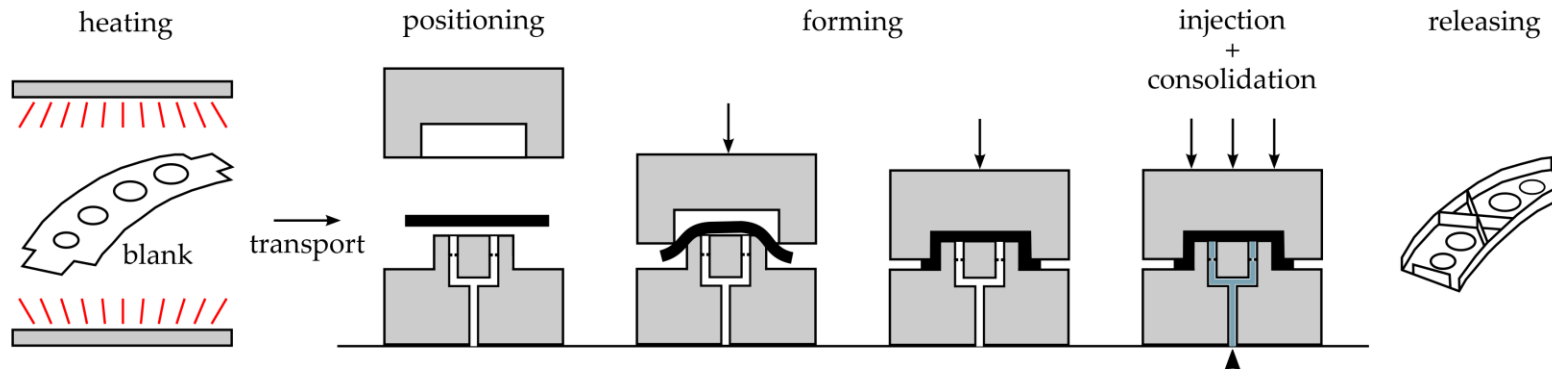


Photo: TPRC



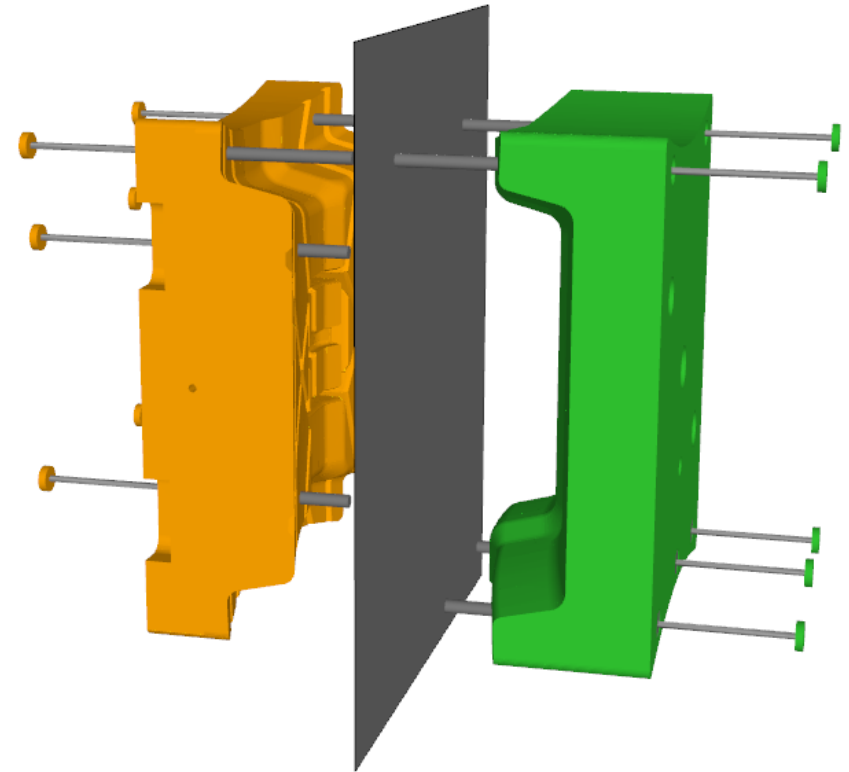
Case study 2 – Overmolding demonstrator

Laminate

- Toray Cetex® TC1225 (carbon fiber/PAEK) unidirectional tape
- Cross-ply layup $[[0/90]_4/0]$

Identification of laminate contour

- Dimensions limited by injection molding cavity
- Rectangular laminate to determine deformed shape



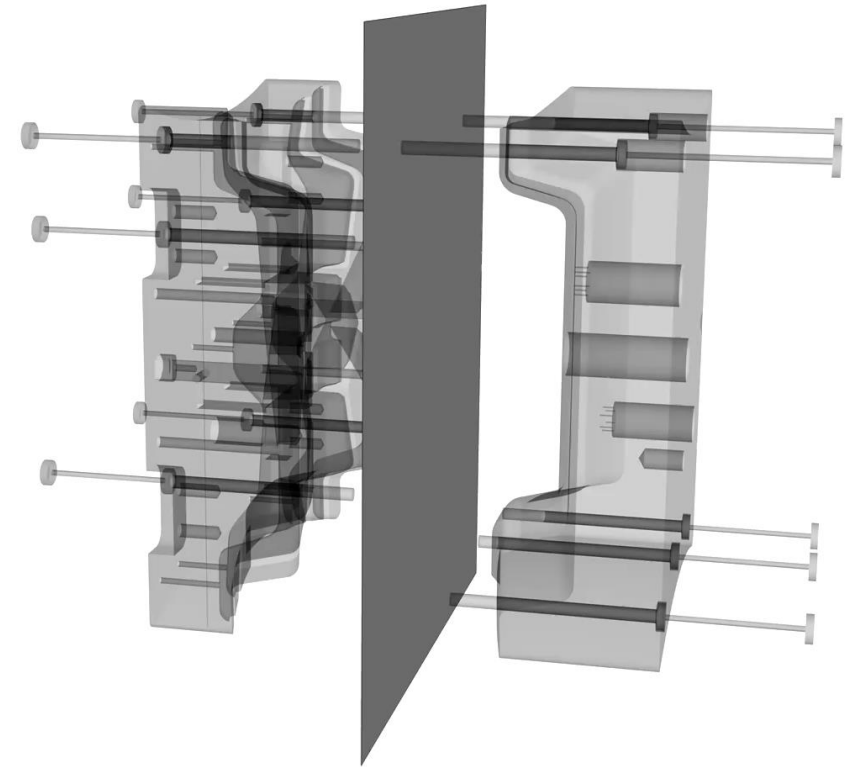
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Y
X
Z
Step: 0
Time: 0
Loadblock: 0 of 0
Progress: 0.0 %

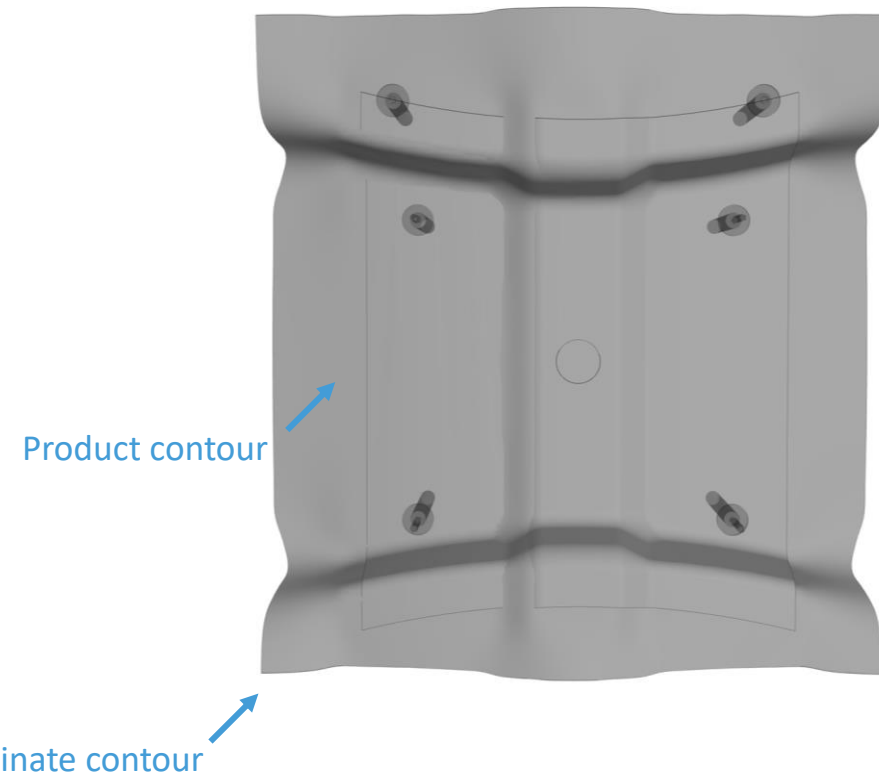
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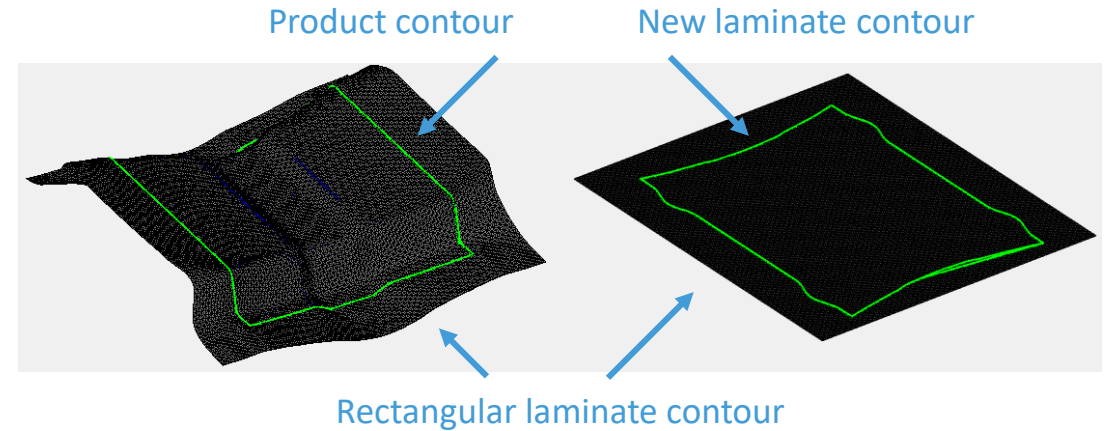
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- AniForm InverseDrape add-on
 - Export of newly created laminate contour



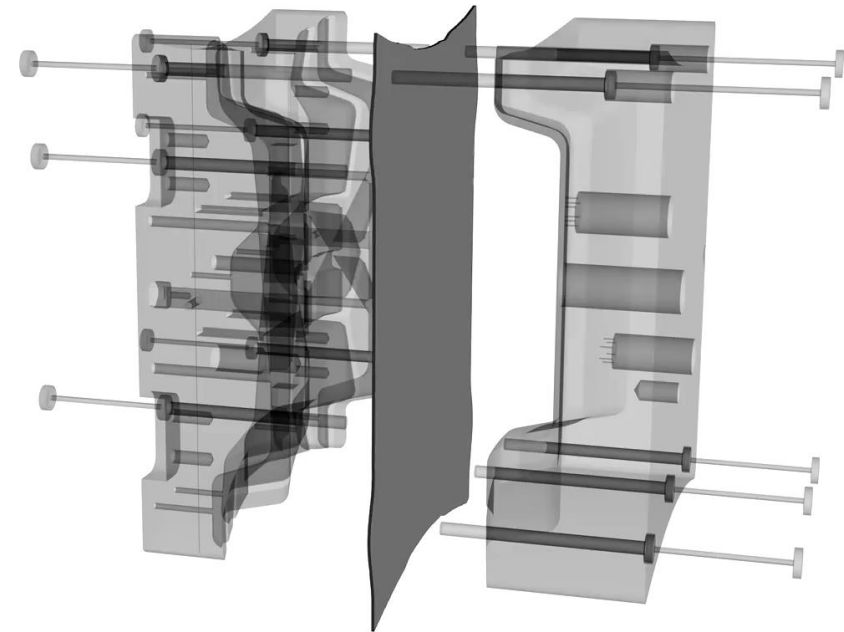
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Y
X
Z
Step: 0
Time: -
Loadblock: - of -
Progress: - %

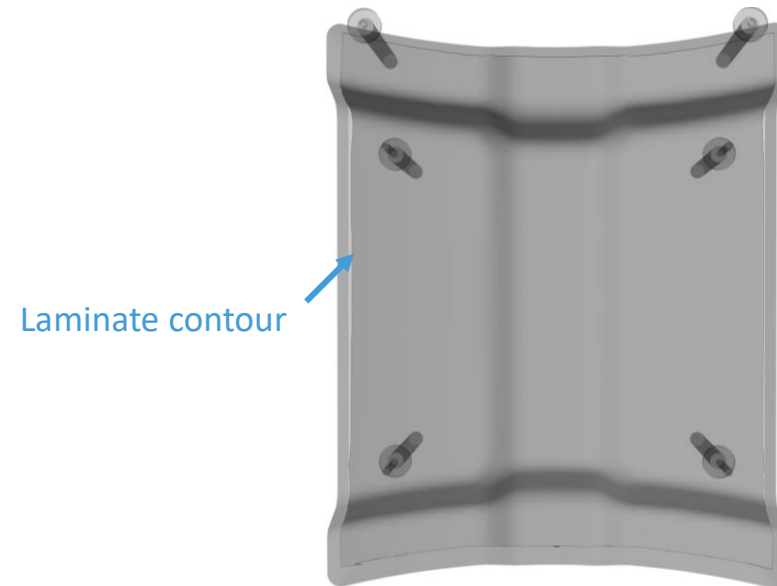
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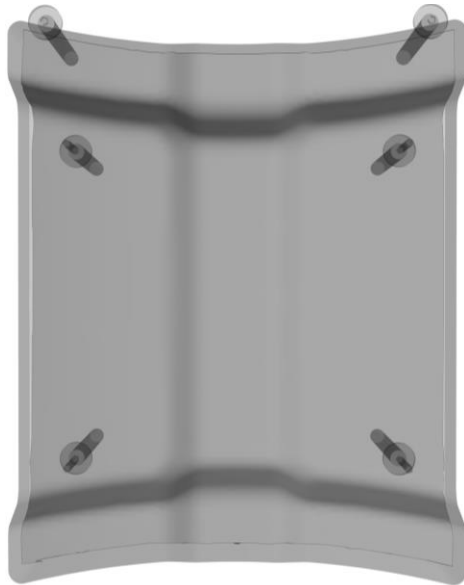
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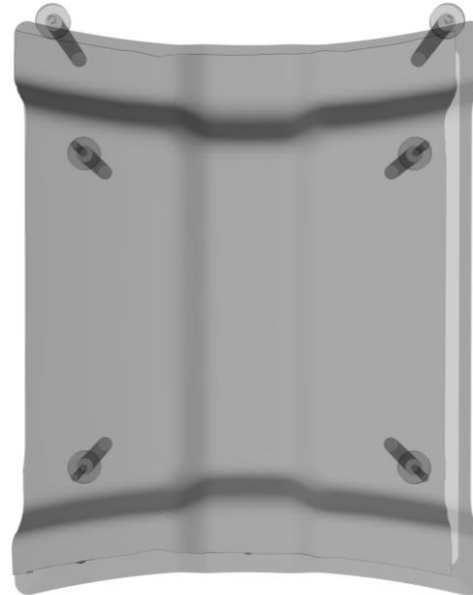
Case study 2 – Overmolding demonstrator

Required accuracy for blank alignment prior to tool closure

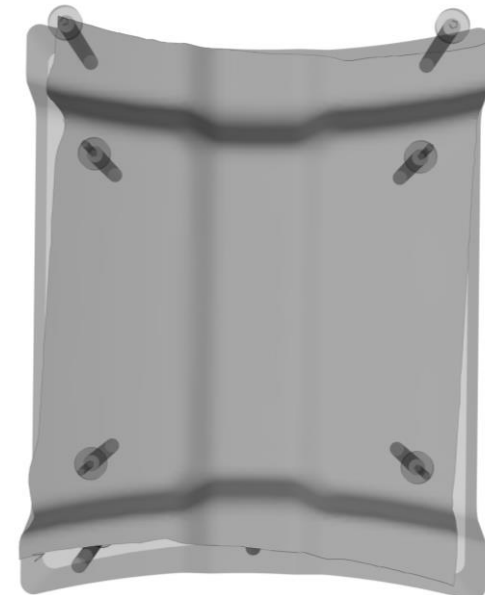
- Laminate cutting by tooling
- Obstruction of polymer flow can result in inadequate filling



Nominal



5 mm horizontal translation



3° rotation around product normal axis

Case study 3 – Deep box with concave & convex flanges

Goal

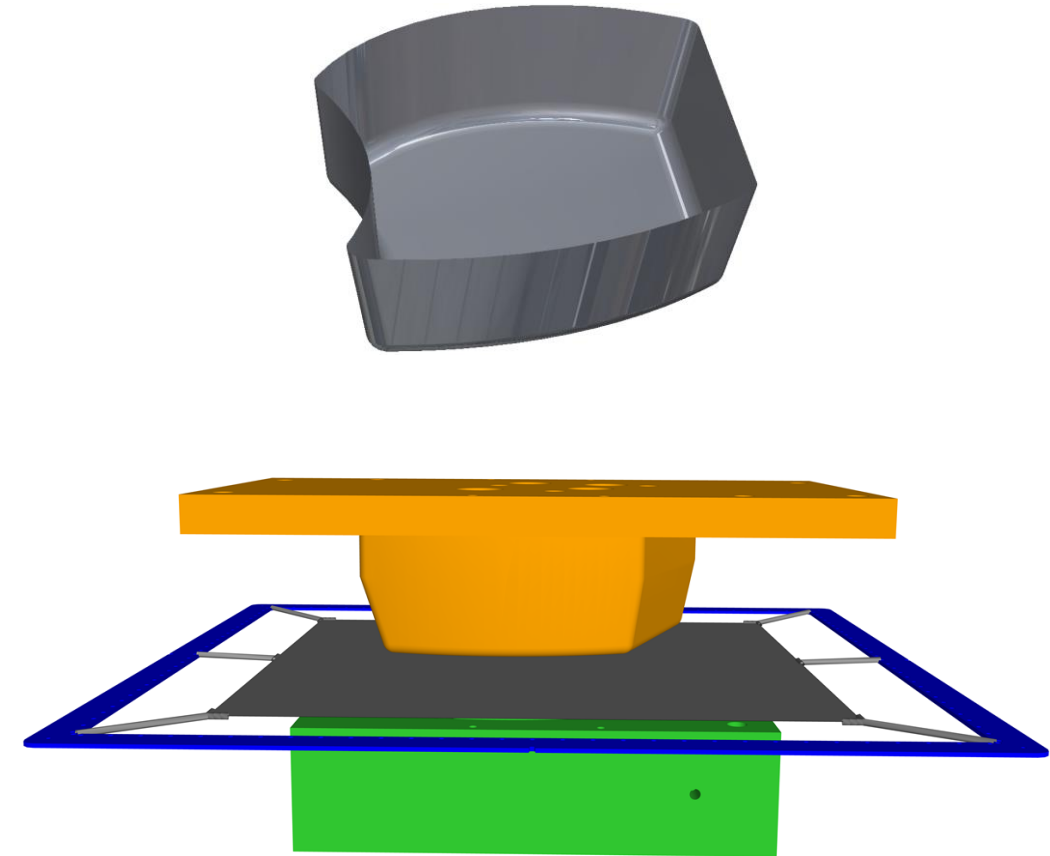
- Optimize for minimal wrinkle formation

Laminate

- Woven carbon fiber/PPS (Toray Cetex[®] TC1100 T300J-5HS/PPS)
- Four plies quasi-isotropic [(45/-45), (0/90)]_s & cross-ply [(0/90)]_{2s}
- 470 x 470 mm

Boundary conditions

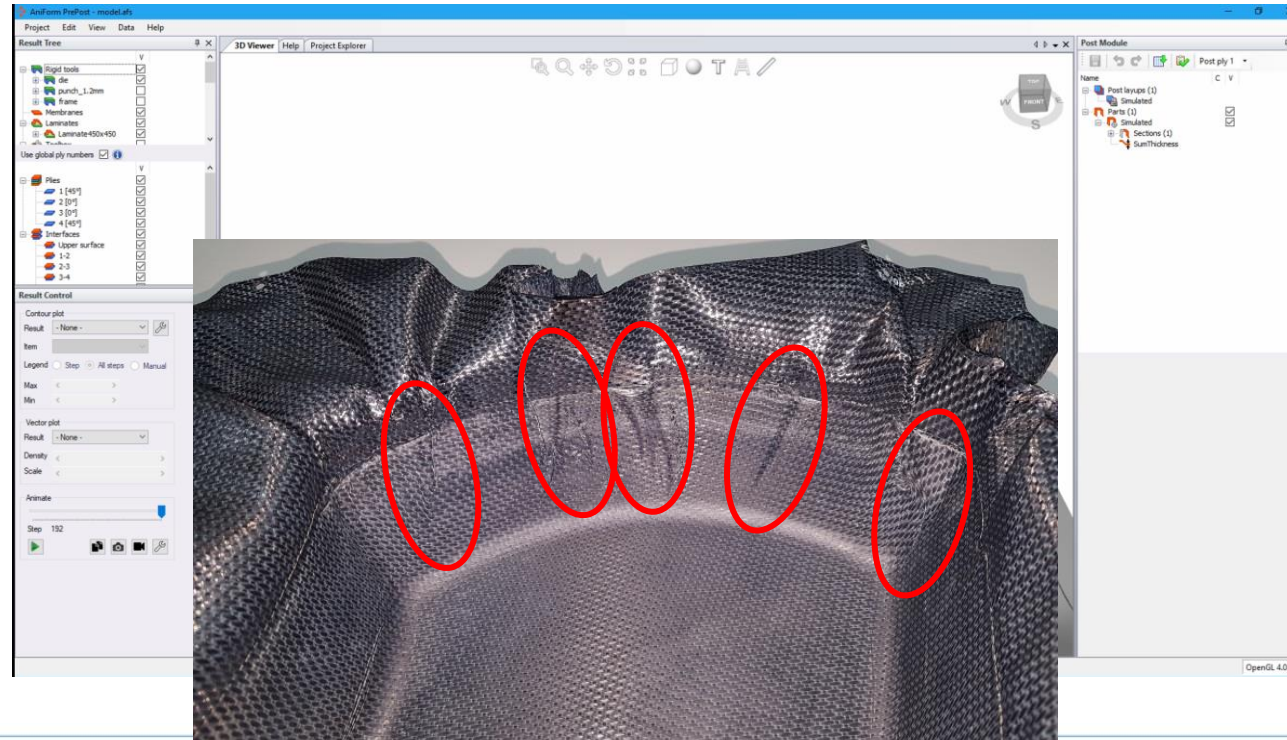
- Male (moving) and female (fixed) tooling
- Handling system via edge grippers and tensioners (springs)



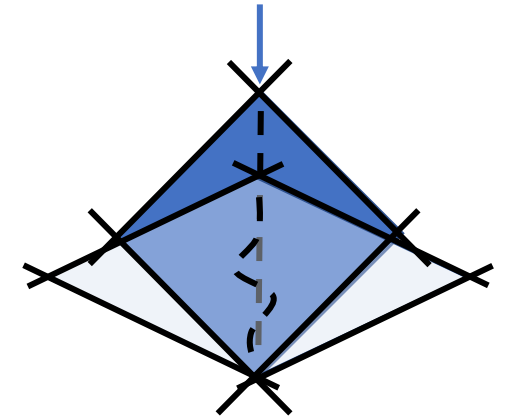
Case study 3 – Deep box with concave & convex flanges

Results

- Wrinkle formation near edge for quasi-isotropic [(45/-45), (0/90)]_s laminate
 - Impediment of in-plane shearing due to presence of adjacent fibers



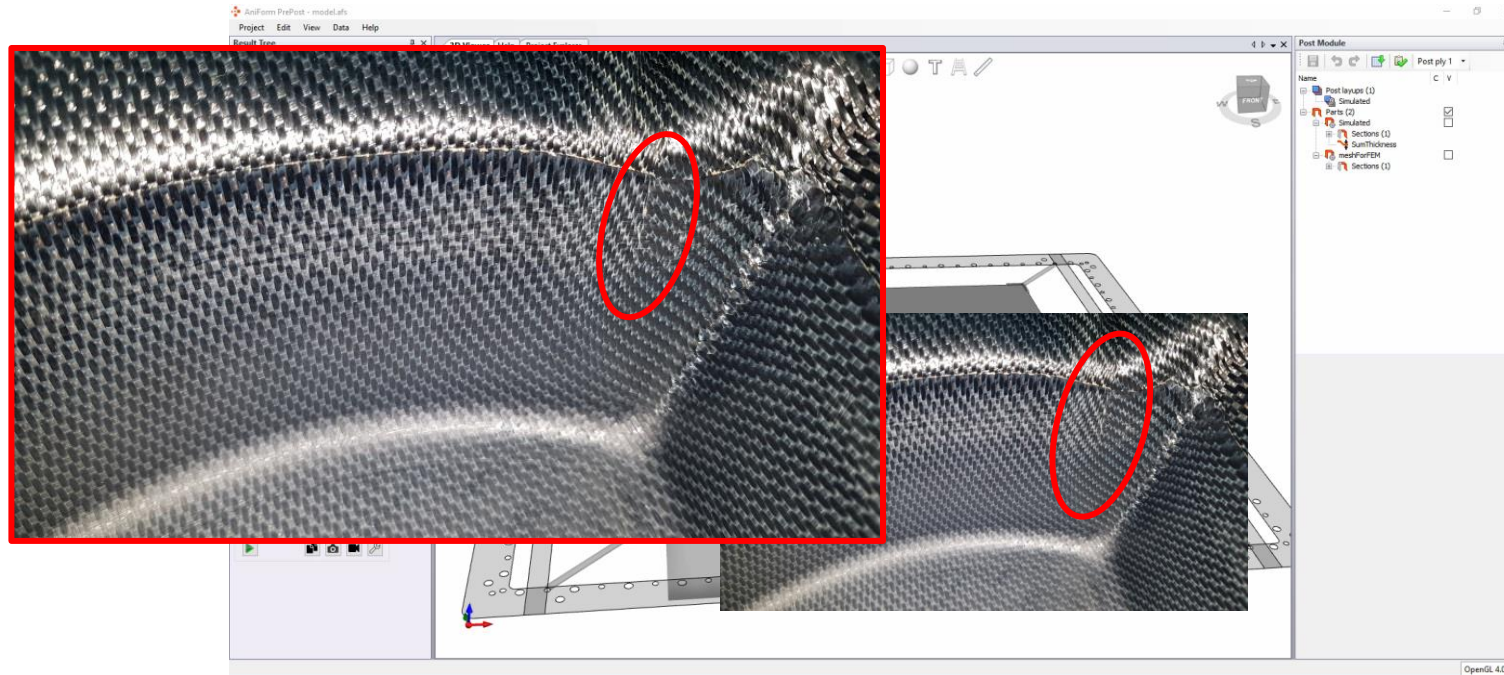
Fiber compression in adjacent ply in shearing direction



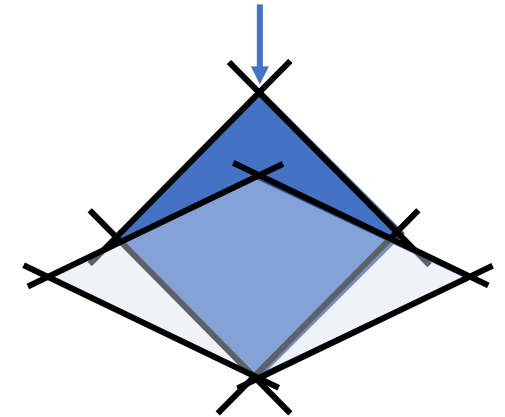
Case study 3 – Deep box with concave & convex flanges

Results

- Wrinkle reduction for cross-ply $[(0/90)]_{2s}$ however not fully resolved
 - In-plane shear deformation is promoted



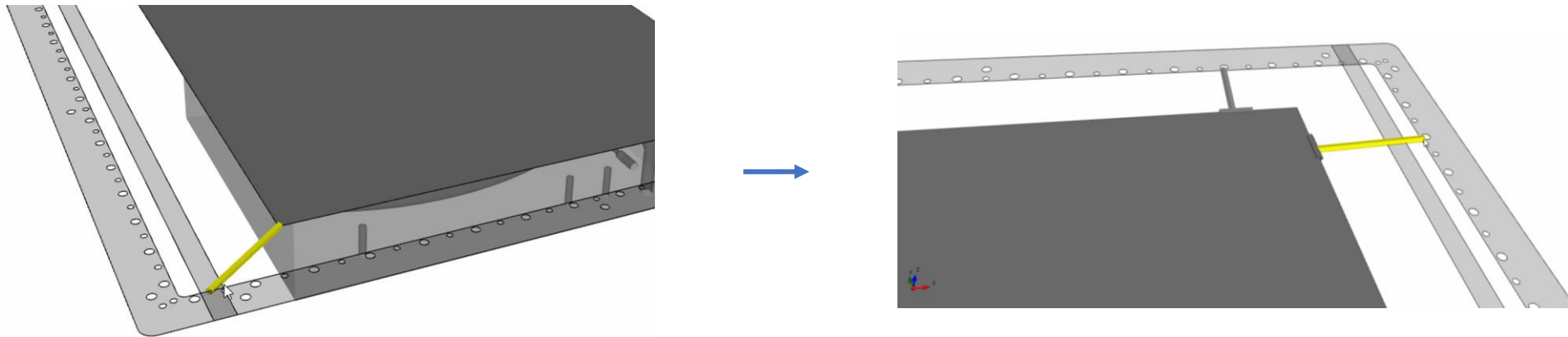
No fiber compression in adjacent ply in shearing direction



Case study 3 – Deep box with concave & convex flanges

Results

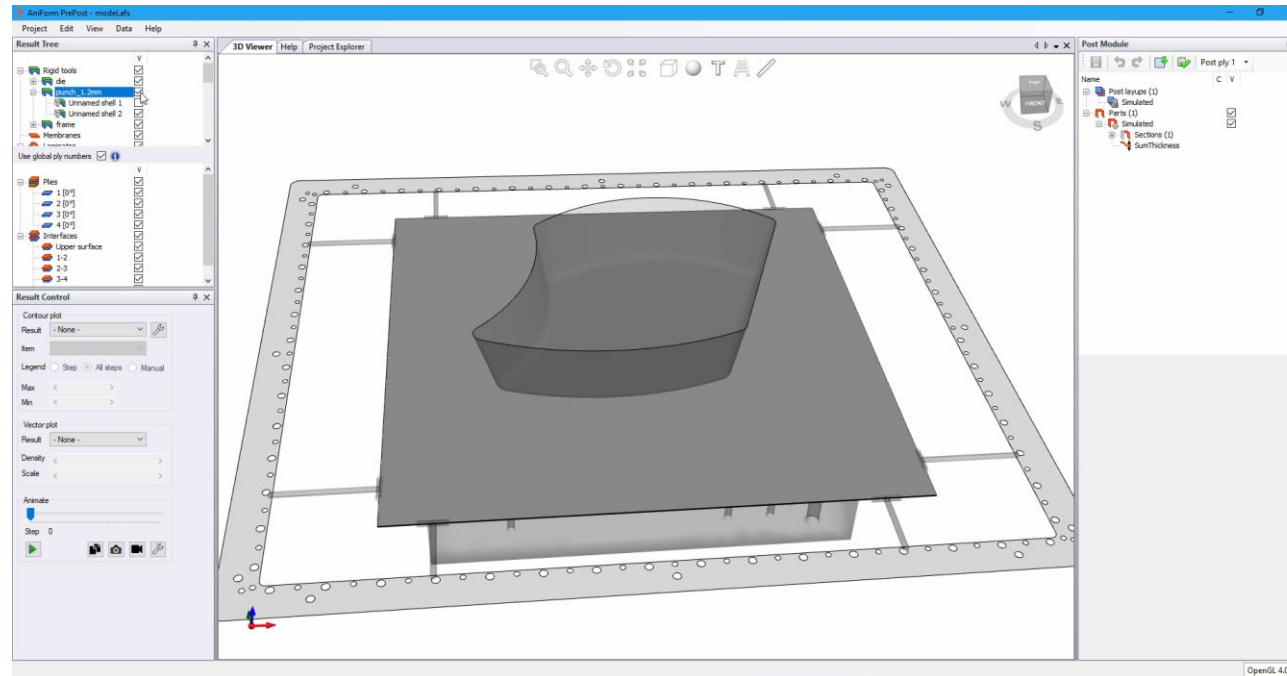
- Change handling system to minimize localization of shear
 - Decoupling the tensioners introduces shear over a larger area



Case study 3 – Deep box with concave & convex flanges

Results

- Change handling system to minimize localization of shear
 - Decoupling the tensioners introduces shear over a larger area



Case study 3 – Deep box with concave & convex flanges



Summary

The following was achieved in the cases discussed:

- identify regions prone to fiber tensioning and compression and their relation to part-size;
- determine near net-shape laminate contour and identify potential blank alignment issues;
- optimize for minimal wrinkle formation.

State-of-the-art simulation techniques:

- provide useful insights of forming-induced phenomena;
- enable investigation of their sensitivity to various process configurations;
- and eventually contribute to finding the optimal solution.

Thank you for your attention

Questions?

t.donderwinkel@aniform.com
aniform.com



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